

Fundamentals of Microelectronics

- CH1 Why Microelectronics?
- CH2 Basic Physics of Semiconductors
- CH3 Diode Circuits
- CH4 Physics of Bipolar Transistors
- CH5 Bipolar Amplifiers
- CH6 Physics of MOS Transistors
- CH7 CMOS Amplifiers
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Chapter 4 Physics of Bipolar Transistors

- 4.1 General Considerations
- 4.2 Structure of Bipolar Transistor
- 4.3 Operation of Bipolar Transistor in Active Mode
- 4.4 Bipolar Transistor Models
- 4.5 Operation of Bipolar Transistor in Saturation Mode
- 4.6 The PNP Transistor

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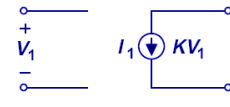
Bipolar Transistor

Voltage-Controlled Device as Amplifying Element \Rightarrow Structure of Bipolar Transistor \Rightarrow Operation of Bipolar Transistor \Rightarrow Large-Signal Model \Rightarrow Small-Signal Model

➤ **In the chapter, we will study the physics of bipolar transistor and derive large and small signal models.**

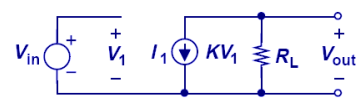
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Voltage-Dependent Current Source

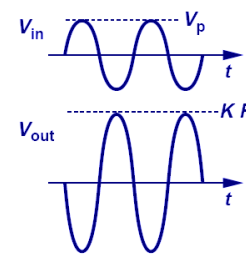


(a)

$$A_v = \frac{V_{out}}{V_{in}} = -KR_L$$



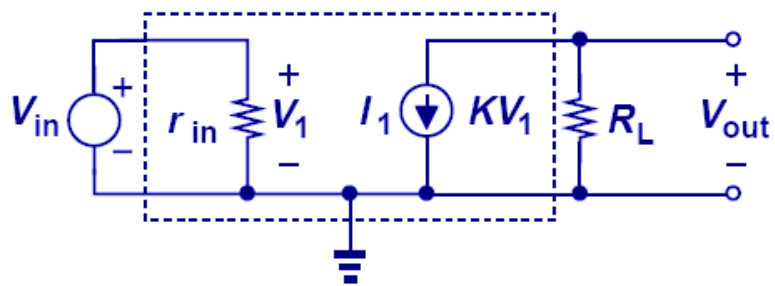
(b)



➤ **A voltage-dependent current source can act as an amplifier.**
➤ **If KRL is greater than 1, then the signal is amplified.**

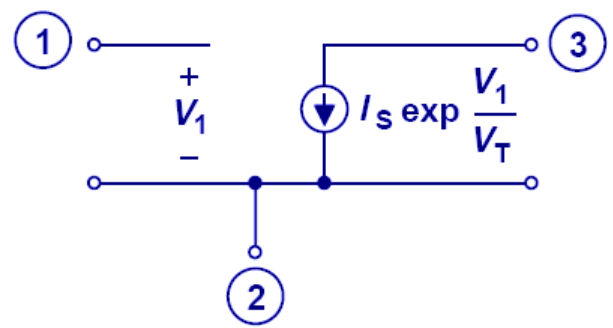
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Voltage-Dependent Current Source with Input Resistance



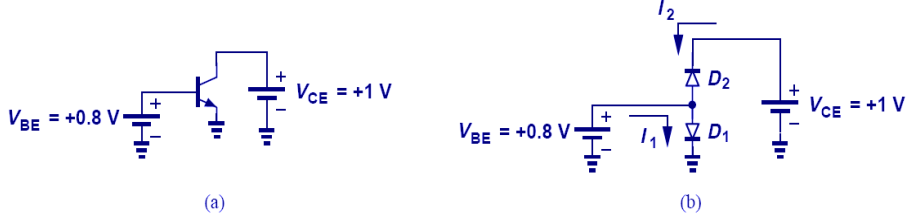
➤ **Regardless of the input resistance, the magnitude of amplification remains unchanged.**

Exponential Voltage-Dependent Current Source



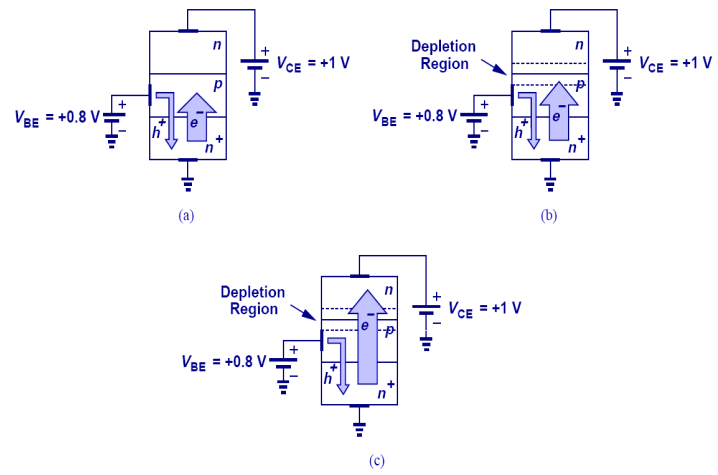
➤ **A three-terminal exponential voltage-dependent current source is shown above.**
 ➤ **Ideally, bipolar transistor can be modeled as such.**

Forward Active Region



- Forward active region: $V_{BE} > 0, V_{BC} < 0$.
- Figure b) presents a WRONG way of modeling figure a).

Accurate Bipolar Representation



- Collector also carries current due to carrier injection from base.

Carrier Transport in Base

(a) Forward Biased (b) Reverse Biased (c) Electron Density

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Collector Current

$$I_C = \frac{A_E q D_n n_i^2}{N_E W_B} \left(\exp \frac{V_{BE}}{V_T} - 1 \right)$$

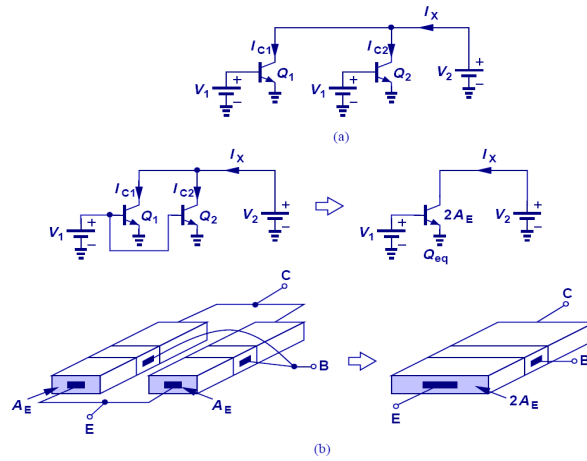
$$I_C = I_S \exp \frac{V_{BE}}{V_T}$$

$$I_S = \frac{A_E q D_n n_i^2}{N_E W_B}$$

- Applying the law of diffusion, we can determine the charge flow across the base region into the collector.
- The equation above shows that the transistor is indeed a voltage-controlled element, thus a good candidate as an amplifier.

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Parallel Combination of Transistors

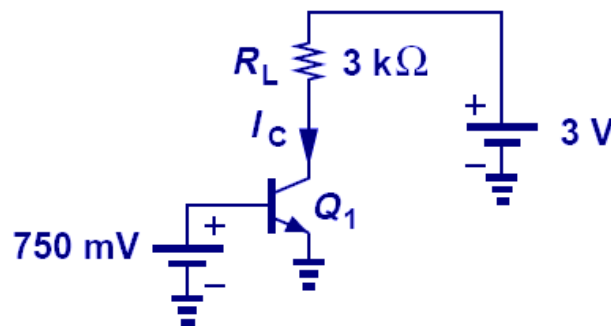


- When two transistors are put in parallel and experience the same potential across all three terminals, they can be thought of as a single transistor with twice the emitter area.

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Simple Transistor Configuration

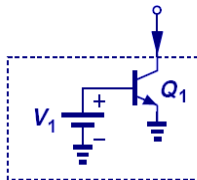
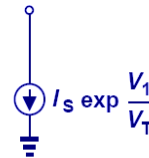
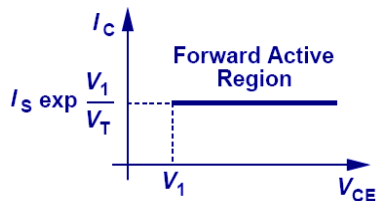


- Although a transistor is a voltage to current converter, output voltage can be obtained by inserting a load resistor at the output and allowing the controlled current to pass thru it.

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Constant Current Source

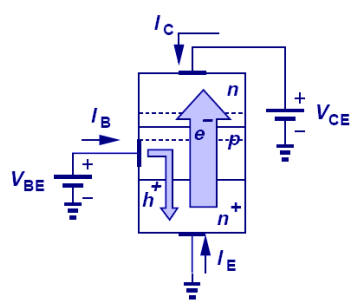
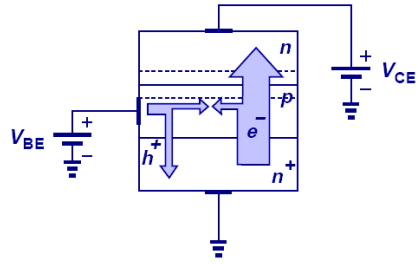




➤ Ideally, the collector current does not depend on the collector to emitter voltage. This property allows the transistor to behave as a constant current source when its base-emitter voltage is fixed.

BJT Modes of Operation		
Mode	EBJ	CBJ
Cutoff	Reverse	Reverse
Active	Forward	Reverse
Saturation	Forward	Forward

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Base Current

$$I_C = \beta I_B$$

➤ Base current consists of two components: 1) Reverse injection of holes into the emitter and 2) recombination of holes with electrons coming from the emitter.

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Emitter Current

$$I_E = I_C + I_B$$

$$I_E = I_C \left(1 + \frac{1}{\beta} \right)$$

$$\beta = \frac{I_C}{I_B}$$

- Applying Kirchoff's current law to the transistor, we can easily find the emitter current.

Summary of Currents

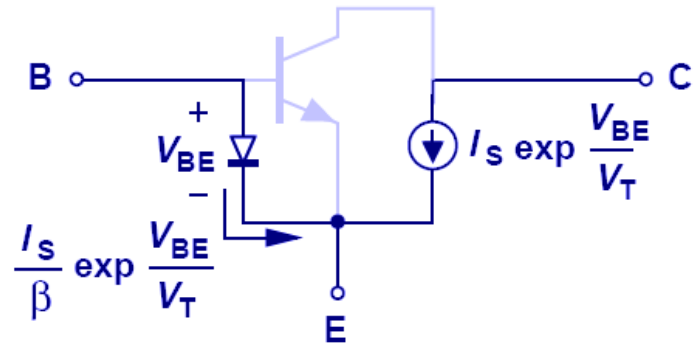
$$I_C = I_S \exp \frac{V_{BE}}{V_T}$$

$$I_B = \frac{1}{\beta} I_S \exp \frac{V_{BE}}{V_T}$$

$$I_E = \frac{\beta + 1}{\beta} I_S \exp \frac{V_{BE}}{V_T}$$

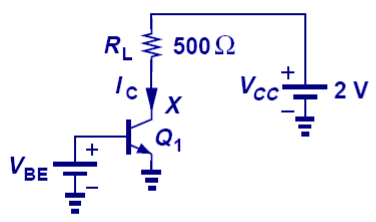
$$\frac{\beta}{\beta + 1} = \alpha$$

Bipolar Transistor Large Signal Model

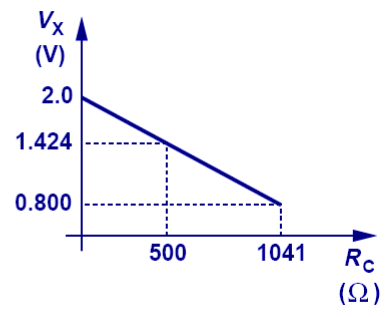


- A diode is placed between base and emitter and a voltage controlled current source is placed between the collector and emitter.

Example: Maximum R_L



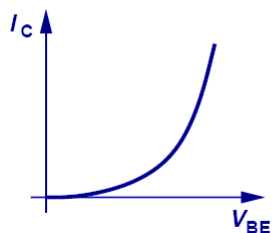
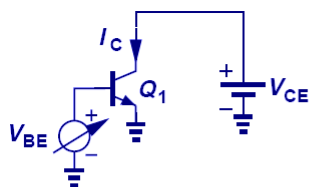
(a)



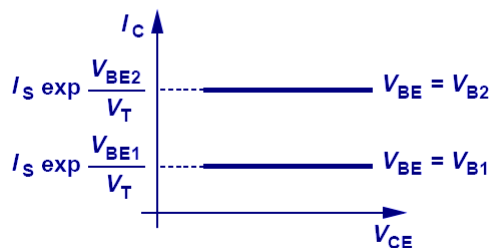
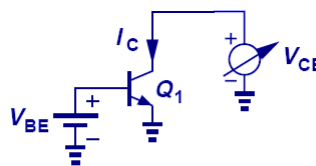
(b)

- As R_L increases, V_x drops and eventually forward biases the collector-base junction. This will force the transistor out of forward active region.
- Therefore, there exists a maximum tolerable collector resistance.

Characteristics of Bipolar Transistor



(a)

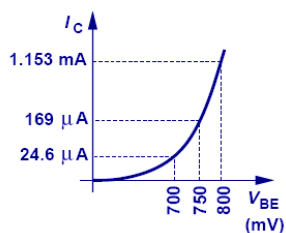


(b)

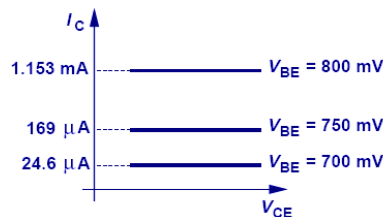
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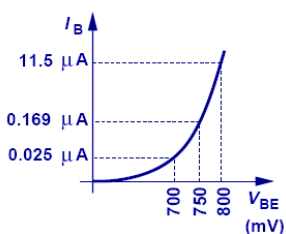
Example: IV Characteristics



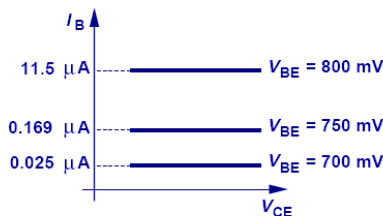
(a)



(b)



(c)

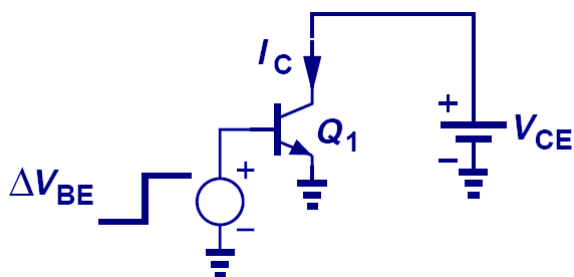


(d)

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Transconductance



$$g_m = \frac{d}{dV_{BE}} \left(I_S \exp \frac{V_{BE}}{V_T} \right)$$

$$g_m = \frac{1}{V_T} I_S \exp \frac{V_{BE}}{V_T}$$

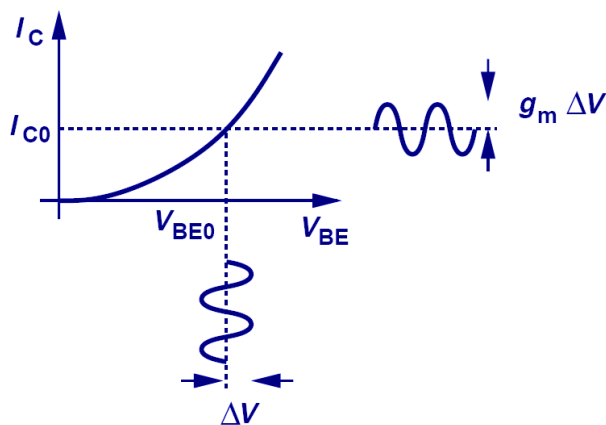
$$g_m = \frac{I_C}{V_T}$$

- Transconductance, g_m shows a measure of how well the transistor converts voltage to current.
- It will later be shown that g_m is one of the most important parameters in circuit design.

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Visualization of Transconductance

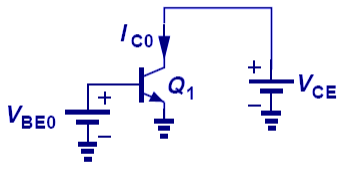


- g_m can be visualized as the slope of I_C versus V_{BE} .
- A large I_C has a large slope and therefore a large g_m .

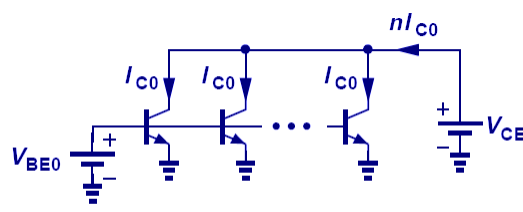
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Transconductance and Area



(a)

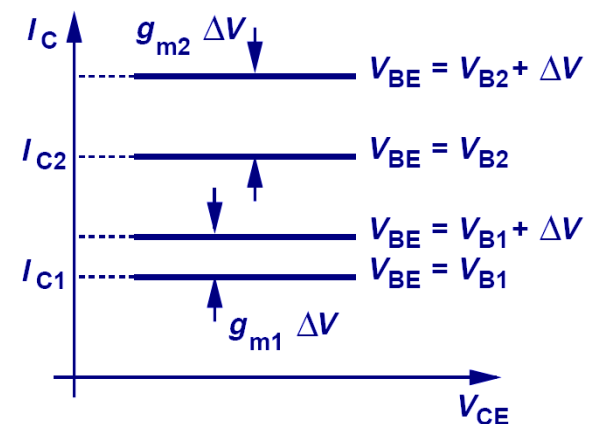


(b)

➤ When the area of a transistor is increased by n , I_S increases by n . For a constant V_{BE} , I_C and hence g_m increases by a factor of n .

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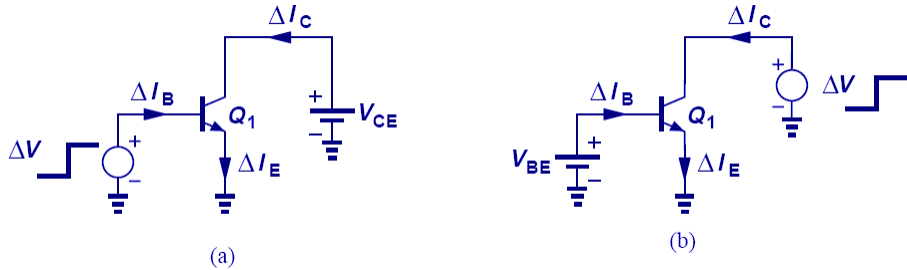
Transconductance and I_c



➤ The figure above shows that for a given V_{BE} swing, the current excursion around I_{C2} is larger than it would be around I_{C1} . This is because g_m is larger I_{C2} .

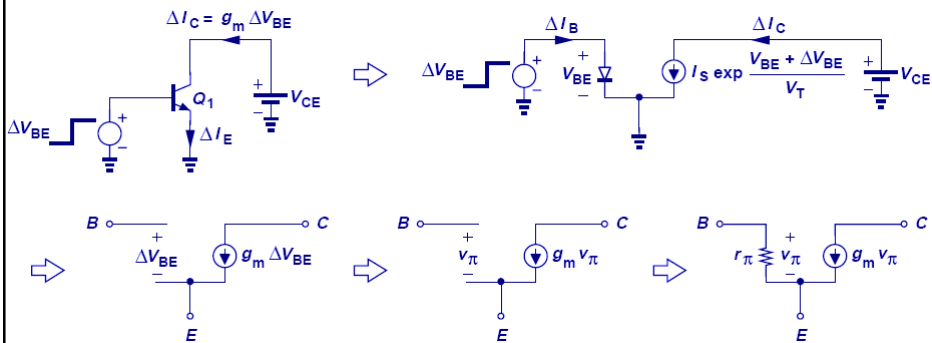
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Small-Signal Model: Derivation

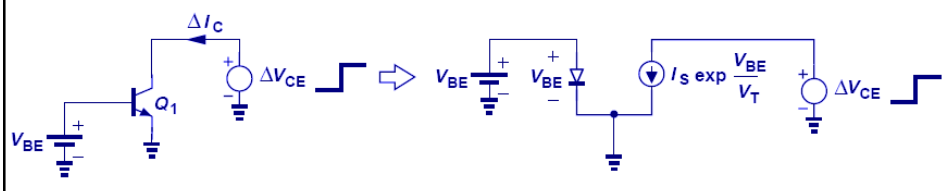


➤ **Small signal model is derived by perturbing voltage difference every two terminals while fixing the third terminal and analyzing the change in current of all three terminals. We then represent these changes with controlled sources or resistors.**

Small-Signal Model: V_{BE} Change

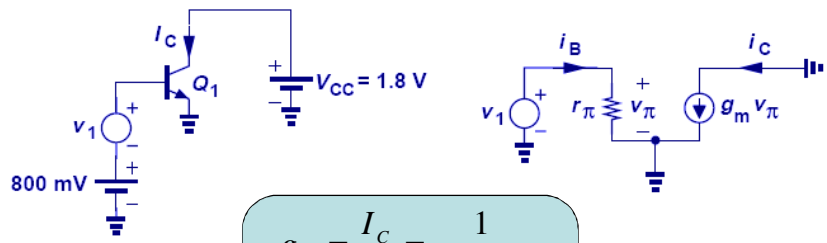


Small-Signal Model: V_{CE} Change



- Ideally, V_{CE} has no effect on the collector current. Thus, it will not contribute to the small signal model.
- It can be shown that V_{CB} has no effect on the small signal model, either.

Small Signal Example I

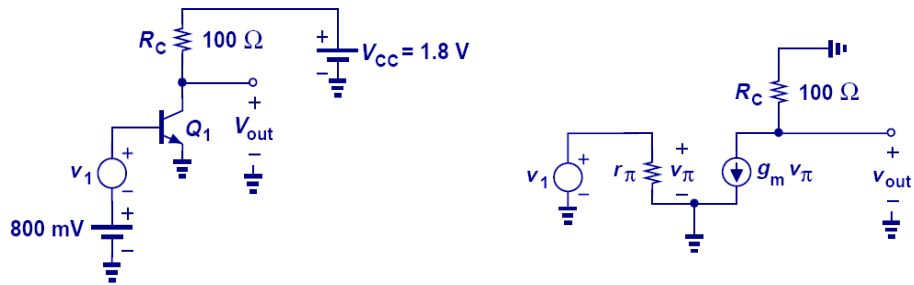


$$g_m = \frac{I_C}{V_T} = \frac{1}{3.75 \Omega}$$

$$r_\pi = \frac{\beta}{g_m} = 375 \Omega$$

- Here, small signal parameters are calculated from DC operating point and are used to calculate the change in collector current due to a change in V_{BE} .

Small Signal Example II



- In this example, a resistor is placed between the power supply and collector, therefore, providing an output voltage.

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AC Ground

- Since the power supply voltage does not vary with time, it is regarded as a ground in small-signal analysis.

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Early Effect

The diagram shows two bipolar transistors in common-emitter configuration. Both have a base-emitter voltage V_{BE} and a collector-emitter voltage V_{CE} . The left transistor is at V_{CE1} and has depletion widths x_1 and x_2 between the base and emitter, and between the base and collector, respectively. The right transistor is at a higher V_{CE2} . Its depletion width between the base and collector is larger, x'_2 , which reduces the effective base width from x_1 to x'_1 . This reduction in base width increases the collector current.

- The claim that collector current does not depend on VCE is not accurate.
- As VCE increases, the depletion region between base and collector increases. Therefore, the effective base width decreases, which leads to an increase in the collector current.

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Early Effect Illustration

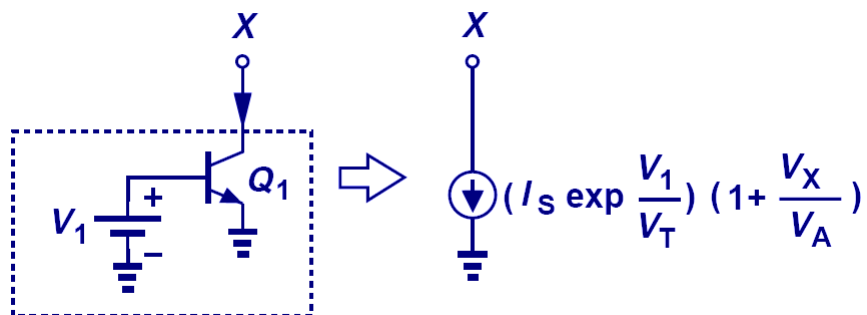
Graph (a) shows the collector current I_C versus the base-emitter voltage V_{BE} . The solid curve represents the transistor with the Early Effect, showing a steeper increase in I_C for a given V_{BE} compared to the dashed curve, which represents the transistor without the Early Effect.

Graph (b) shows the collector current I_C versus the collector-emitter voltage V_{CE} . The solid line represents the transistor with the Early Effect, showing that I_C increases with V_{CE} . The dashed horizontal line represents the transistor without the Early Effect, where I_C is constant and equal to $I_S \exp\left(\frac{V_{BE1}}{V_T}\right)$.

- With Early effect, collector current becomes larger than usual and a function of VCE.

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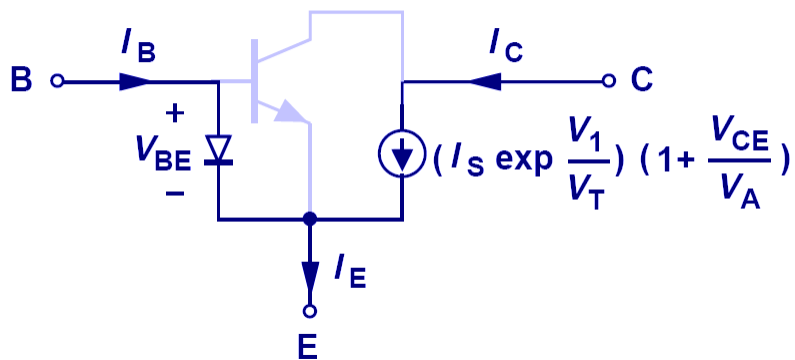
Early Effect Representation



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Early Effect and Large-Signal Model

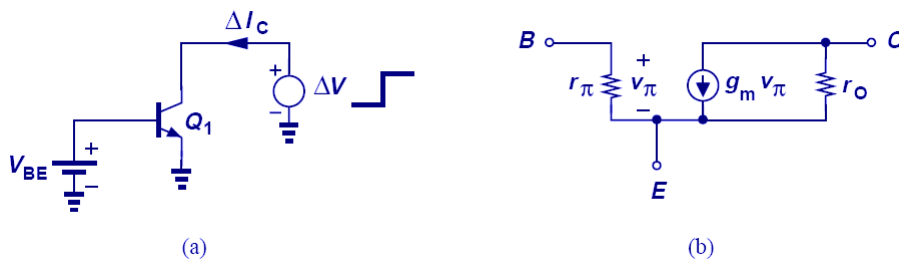


- Early effect can be accounted for in large-signal model by simply changing the collector current with a correction factor.
- In this mode, base current does not change.

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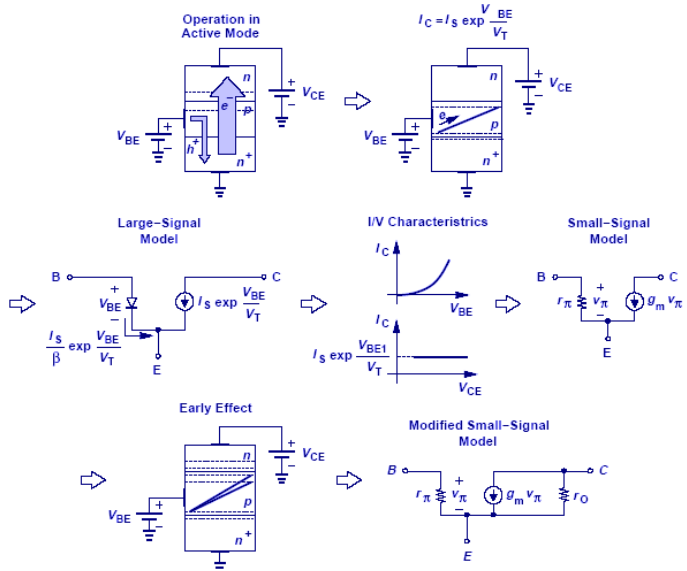
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Early Effect and Small-Signal Model

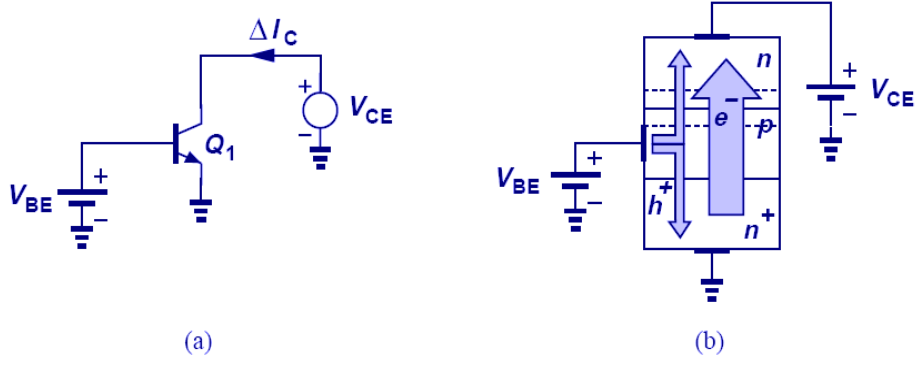


$$r_o = \frac{\Delta V_{CE}}{\Delta I_C} = \frac{V_A}{I_S \exp \frac{V_{BE}}{V_T}} \approx \frac{V_A}{I_C}$$

Summary of Ideas

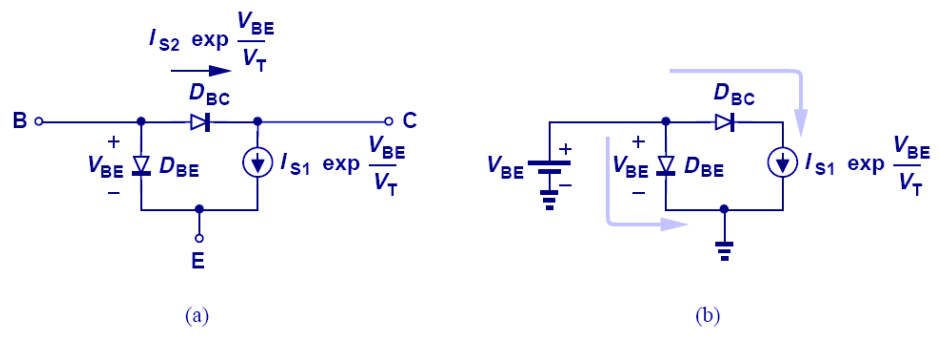


Bipolar Transistor in Saturation

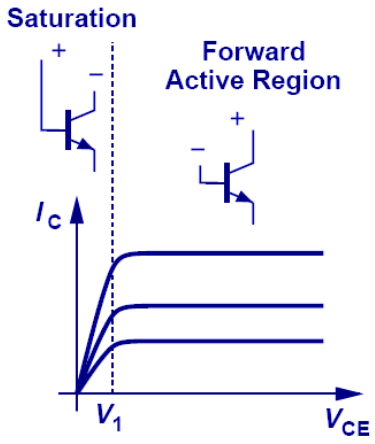


➤ When collector voltage drops below base voltage and forward biases the collector-base junction, base current increases and decreases the current gain factor, β .

Large-Signal Model for Saturation Region

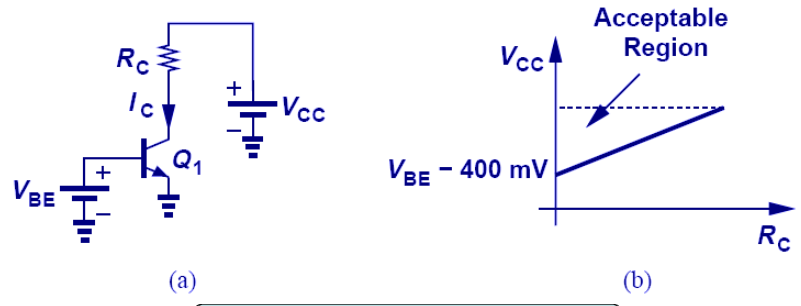


Overall I/V Characteristics



➤ The speed of the BJT also drops in saturation.

Example: Acceptable V_{CC} Region



$$V_{CC} \geq I_C R_C + (V_{BE} - 400\text{ mV})$$

- In order to keep BJT at least in soft saturation region, the collector voltage must not fall below the base voltage by more than 400mV.
- A linear relationship can be derived for V_{CC} and R_C and an acceptable region can be chosen.

Deep Saturation

➤ In deep saturation region, the transistor loses its voltage-controlled current capability and V_{CE} becomes constant.

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PNP Transistor

(a)

(b)

(c)

(d)

➤ With the polarities of emitter, collector, and base reversed, a PNP transistor is formed.

➤ All the principles that applied to NPN's also apply to PNP's, with the exception that emitter is at a higher potential than base and base at a higher potential than collector.

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A Comparison between NPN and PNP Transistors

(a)

Active Mode	Edge of Saturation	Saturation Mode
	(a)	
Active Mode	Edge of Saturation	Saturation Mode
	(b)	

➤ The figure above summarizes the direction of current flow and operation regions for both the NPN and PNP BJT's.

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PNP Equations

$$I_C = I_S \exp \frac{V_{EB}}{V_T}$$

$$I_B = \frac{I_S}{\beta} \exp \frac{V_{EB}}{V_T}$$

$$I_E = \frac{\beta + 1}{\beta} I_S \exp \frac{V_{EB}}{V_T}$$

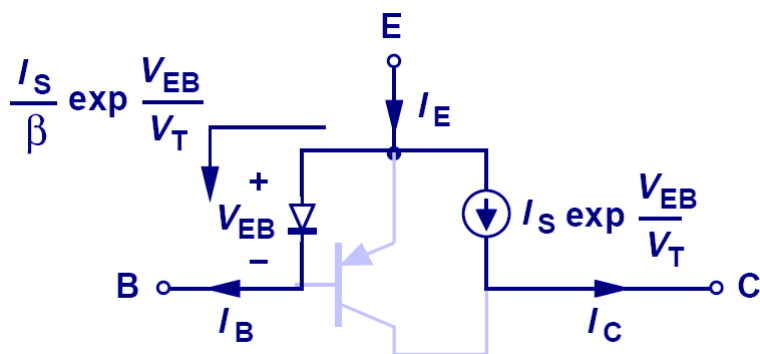
Early Effect

➔

$$I_C = \left(I_S \exp \frac{V_{EB}}{V_T} \right) \left(1 + \frac{V_{EC}}{V_A} \right)$$

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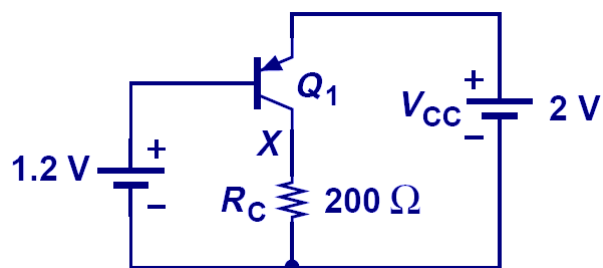
Large Signal Model for PNP



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PNP Biasing

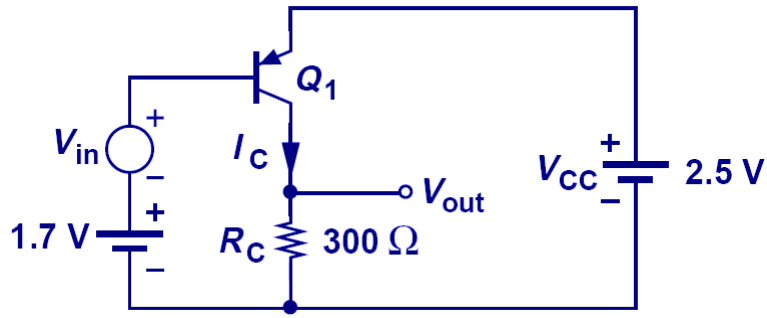


➤ Note that the emitter is at a higher potential than both the base and collector.

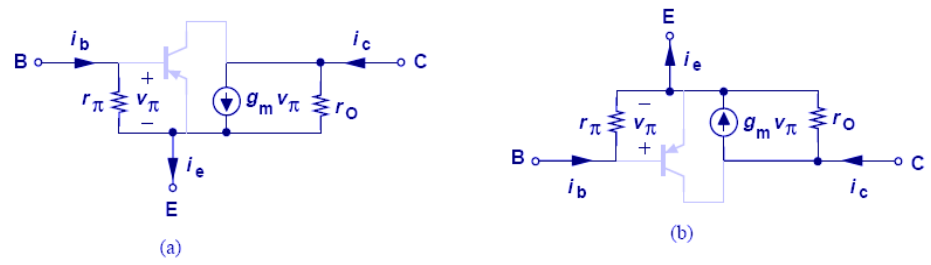
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Small Signal Analysis

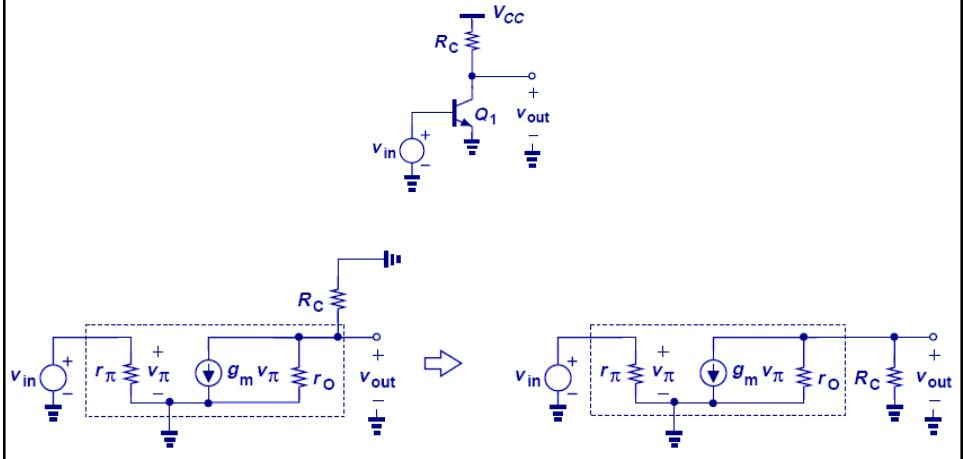


Small-Signal Model for PNP Transistor

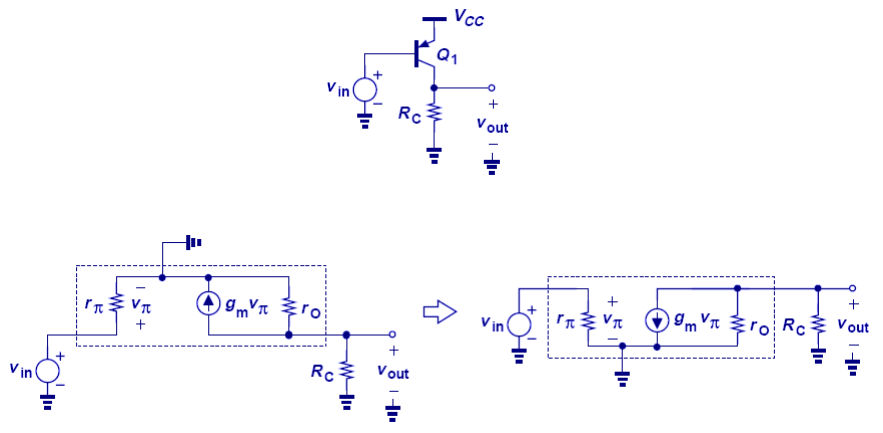


➤ **The small signal model for PNP transistor is exactly IDENTICAL to that of NPN. This is not a mistake because the current direction is taken care of by the polarity of V_{BE}.**

Small Signal Model Example I

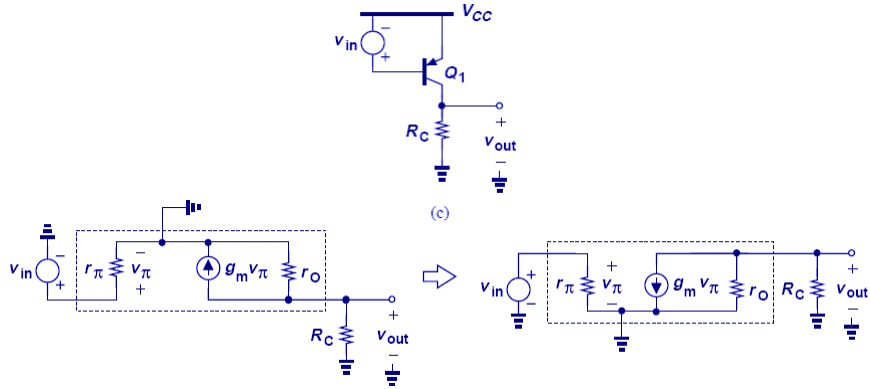


Small Signal Model Example II



➤ Small-signal model is identical to the previous ones.

Small Signal Model Example III



➤ Since during small-signal analysis, a constant voltage supply is considered to be AC ground, the final small-signal model is identical to the previous two.

Small Signal Model Example IV

